## Orbit Options for Near-Term Space Solar Power

Seth D. Potter, Ph.D.<br>SDP Space Systems<br>Redondo Beach, CA

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## Introduction

- Studies of space solar power (SSP) for the commercial grid have usually considered transmitting power from geostationary orbit (GEO), via microwaves at frequencies below 10 GHz , where the atmosphere is relatively transparent.
- Due to beam divergence from that distance at such frequencies, system sizes must be large, leading to power levels of 1000 MW or more
- The scale of the systems makes competing with traditional energy sources challenging
- Recent studies have considered SSP for nearer-term niche uses in remote locations
- Many remote locations are typically powered by generators, which depend on fuel delivered at great cost, often through hazardous environments.
- Power requirements for such users may range from a few hundred kilowatts to several megawatts.
- Some remote facilities are at high latitudes, which are inaccessible from geostationary orbit, so orbits that are lower, and/or elliptical, will be considered
- Since non-GEO orbits do not remain over their intended ground sites, systems or constellations, of satellites must be designed, in which beam handoffs can provide a given ground site with power much of the time, while making maximum use of the satellites as multiple satellites serve multiple ground sites


## Location of Potential Ground User Sites

- The number of potential ground sites is potentially unlimited
- For non-GEO orbits, access is largely independent of longitude
- Exceptions are sparse constellations of satellites with repeating ground track orbits, particularly elliptical orbits
- Therefore, three ground regions were chosen:
- Low latitude, within $\pm 10^{\circ}$ of the equator
- Middle latitude, $30^{\circ}$ to $35^{\circ}$
- High latitude, above $60^{\circ}$


## SPS ALPHA: Adaptable to Multiple Orbits



- Solar Power Satellite by means of Arbitrarily Large Phased Array (SPS-ALPHA) concept developed by John C. Mankins, Mankins Space Technology, Inc.; image used with permission
- Shown here in GEO, and can be adapted for low and high inclination Low Earth Orbits


## Constellation Development Process: Ground Rules and Assumptions

- Performed Excel analysis to estimate access times
- $15^{\circ}, 30^{\circ}, 45^{\circ}$ minimum elevation angles considered
- Assumed 90\% coverage duty cycle at ground sites
- $30^{\circ}$ minimum elevation angle selected for further analysis in STK
- $15^{\circ}$ leads to excessive losses due to elongation of beam and increased slant range
- $45^{\circ}$ may be too restrictive in terms of access time, but may be worthwhile, due to lower losses
- Twelve orbits initially considered
- Excel model assumes satellite passes directly over ground site, and ignores Earth's rotation
- Shadowing of satellites not yet considered
- Ran cases for low, middle, and high latitudes
- Orbit propagated for one calendar year starting at vernal equinox of 2028
- $90 \%$ coverage duty cycle retained to estimate number of satellites needed


## Excel Access Time Analysis



- Shadowing not yet considered
- Red numbers indicate that for elliptical orbits, Excel assumed circular orbits having the same semi-major axes, and hence, same periods
- This will tend to underestimate access times for a location under the apogee
- The Excel estimates for maximum time in view are surprisingly good
- Will tend to underestimate for prograde orbits, and overestimate for retrograde orbits (that is, inclination $>90^{\circ}$ )
- Excel will tend to overestimate the total number of satellites needed to achieve a given duty cycle, because it assumes only one pass per day (though this can be changed by the user)


## Excel Access Time Analysis



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- For elliptical orbits, used circular orbits having the same semi-major axes, and hence, same periods
- This will tend to underestimate access times for a location under the apogee of an elliptical orbit
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- Will tend to underestimate for prograde orbits, and overestimate for retrograde orbits (that is, inclination $>90^{\circ}$ )
- Excel will tend to overestimate the total number of satellites needed to achieve a given duty cycle, because it assumes only one pass per day (though this can be changed by the user)


## STK Access Time Analysis for Low Latitudes

|  |  |  |  |  |  | 30 deg min el angle, single sat pass |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Orbit Description | Apogee Altitude (km) | Perigee Altitude (km) | $\begin{array}{\|c} \hline \text { Equivalent } \\ \text { Circular } \\ \text { Altitude } \\ (k m) \\ \hline \end{array}$ | $\begin{gathered} \text { Inclinatio } \\ \mathrm{n}(\mathrm{deg}) \end{gathered}$ | No. Orbits/Day | Min Time in View (min) | $\qquad$ | $\qquad$ | Avg Accesses / Day | Total <br> Access <br> Time $/$ Year <br> $(\mathrm{min})$ | Duty Cycle | \# Sats for <br> 30 deg <br> min el <br> angle |
| LEO | 500.0 | 500.0 | 500.0 | 28.50 | 15.2 | 0.07 | 3.66 | 2.87 | 2.38 | 2,487.77 | 0.005 | 191 |
| Sun Sync Repeat | 1,676.5 | 1,676.5 | 1,676.5 | 102.94 | 12.0 | 9.20 | 10.90 | 10.09 | 2.00 | 7,366.2 | 0.014 | 65 |
| LEO ALPHA | 2,158.6 | 2,158.6 | 2,158.6 | 28.50 | 11.0 | 0.33 | 15.52 | 11.25 | 6.40 | 26,297.9 | 0.050 | 18 |
| Sun Sync Repeat | 2,158.6 | 2,158.6 | 2,158.6 | 105.93 | 11.0 | 8.03 | 12.95 | 10.31 | 3.00 | 11,287.4 | 0.021 | 42 |
| Sun Sync Repeat | 2,719.9 | 2,719.9 | 2,719.9 | 110.06 | 10.0 | 0.12 | 16.21 | 11.62 | 3.59 | 15,227.4 | 0.029 | 32 |
| Sun Sync Repeat | 3,383.6 | 3,383.6 | 3,383.6 | 116.03 | 9.0 | 20.86 | 21.44 | 21.15 | 2.00 | 15,442.3 | 0.029 | 31 |
| CASSIOPeiA | 7414.00 | 963.00 | 4188.50 | 116.60 | 8.0 | 0.68 | 19.42 | 14.64 | 2.52 | 13,486.7 | 0.026 | 36 |
| Low Van Allen Gap | 7,000.0 | 7,000.0 | 7,000.0 | 55.00 | 5.6 | 3.65 | 56.03 | 44.82 | 2.61 | 42,712.2 | 0.081 | 12 |
| High Van Allen Gap | 12,000.0 | 12,000.0 | 12,000.0 | 55.00 | 3.5 | 7.43 | 114.00 | 92.93 | 1.88 | 63,659.1 | 0.121 | 8 |
| Molniya | 39,850.50 | 500.00 | 20,175.25 | 63.55 | 2.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 0.000 | N/A |
| GPS | 20,200.0 | 20,200.0 | 20,200.0 | 55.00 | 2.0 | 8.13 | 389.75 | 231.51 | 1.04 | 88,206 | 0.168 | 6 |
| GEO | 35,786.0 | 35,786.0 | 35,786.0 | $<1$ | 1.0 | 525,600.0 | 525,600.0 | 525,600.0 | 0.00 | 525,600 | 1.000 | 1 |

- Shadowing not yet considered


## STK Access Time Analysis for Middle Latitudes

|  |  |  |  |  |  | 30 deg min el angle, single sat pass |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Orbit Description | Apogee Altitude (km) | Perigee Altitude (km) | Equivalent <br> Circular <br> Altitude <br> (km) | Inclination (deg) | No. Orbits/Day | Min Time in View (min) | Max Time in View (min) | Avg Time in View (min) | Avg <br> Accesses <br> / Day | Total Access Time / Year (min) | Duty Cycle | \# Sats for 30 deg min el angle |
| LEO | 500.0 | 500.0 | 500.0 | 28.50 | 15.2 | 0.12 | 2.75 | 2.13 | 1.96 | 1,525.89 | 0.0029 | 311 |
| Sun Sync Repeat | 1,676.5 | 1,676.5 | 1,676.5 | 102.94 | 12.0 | 7.59 | 10.37 | 8.65 | 3.00 | 9,472.5 | 0.0180 | 50 |
| LEO ALPHA | 2,158.6 | 2,158.6 | 2,158.6 | 28.50 | 11.0 | 0.48 | 15.11 | 12.58 | 3.92 | 17,969.9 | 0.0342 | 27 |
| Sun Sync Repeat | 2,158.6 | 2,158.6 | 2,158.6 | 105.93 | 11.0 | 6.74 | 13.14 | 10.39 | 4.00 | 15,175.5 | 0.0289 | 32 |
| Sun Sync Repeat | 2,719.9 | 2,719.9 | 2,719.9 | 110.06 | 10.0 | 0.19 | 17.04 | 13.79 | 3.21 | 16,138.1 | 0.0307 | 30 |
| Sun Sync Repeat | 3,383.6 | 3,383.6 | 3,383.6 | 116.03 | 9.0 | 9.90 | 20.99 | 17.03 | 4.00 | 24,865.6 | 0.0473 | 20 |
| CASSIOPeiA | 7414.00 | 963.00 | 4188.50 | 116.60 | 8.0 | 0.70 | 41.44 | 34.41 | 5.40 | 67,855.8 | 0.1291 | 7 |
| Low Van Allen Gap | 7,000.0 | 7,000.0 | 7,000.0 | 55.00 | 5.6 | 7.35 | 56.50 | 49.30 | 3.14 | 56,451.0 | 0.1074 | 9 |
| High Van Allen Gap | 12,000.0 | 12,000.0 | 12,000.0 | 55.00 | 3.5 | 2.09 | 118.41 | 102.80 | 1.97 | 74,019.1 | 0.1408 | 7 |
| Molniya | 39,850.50 | 500.00 | 20,175.25 | 63.55 | 2.0 | 660.73 | 660.73 | 660.73 | 1.00 | 241,826.4 | 0.4601 | 2 |
| GPS | 20,200.0 | 20,200.0 | 20,200.0 | 55.00 | 2.0 | 6.05 | 321.05 | 229.38 | 1.11 | 92,668.6 | 0.1763 | 6 |
| GEO | 35,786.0 | 35,786.0 | 35,786.0 | <1 | 1.0 | 525,600.0 | 525,600.0 | 525,600.0 | 0.00 | 525,600.0 | 1.0000 | 1 |

- Shadowing not yet considered


## STK Access Time Analysis for High Latitudes

|  |  |  |  |  | 30 deg min el angle, single sat pass |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Orbit Description | Apogee Altitude (km) | Perigee Altitude (km) | Inclination (deg) | No. Orbits/Day | Min Time in View (min) | Max Time in View (min) | Avg Time in View (min) | Avg Accesses / Day | Total <br> Access <br> Time / <br> Year (min) | Duty Cycle | \# Sats for <br> 30 deg <br> min el <br> angle |
| LEO | 500.0 | 500.0 | 28.50 | 15.2 | 0.00 | 0.00 | 0.00 | N//A | 0.00 | 0.0000 | N/A |
| Sun Sync Repeat | 1,676.5 | 1,676.5 | 102.94 | 12.0 | 5.87 | 10.97 | 9.23 | 7.00 | 23,587.5 | 0.0449 | 21 |
| LEO ALPHA | 2,158.6 | 2,158.6 | 28.50 | 11.0 | 0.00 | 0.00 | 0.00 | N//A | 0.00 | 0.0000 | N/A |
| Sun Sync Repeat | 2,158.6 | 2,158.6 | 105.93 | 11.0 | 11.54 | 14.06 | 13.02 | 6.00 | 28,506.2 | 0.0542 | 17 |
| Sun Sync Repeat | 2,719.9 | 2,719.9 | 110.06 | 10.0 | 11.71 | 17.45 | 15.58 | 6.00 | 34,123.2 | 0.0649 | 14 |
| Sun Sync Repeat | 3,383.6 | 3,383.6 | 116.03 | 9.0 | 8.00 | 21.75 | 18.27 | 5.00 | 33,336.7 | 0.0634 | 15 |
| CASSIOPeiA | 7414.00 | 963.00 | 116.60 | 8.0 | 1.69 | 54.72 | 45.61 | 5.52 | 91,818.4 | 0.1747 | 6 |
| Low Van Allen Gap | 7,000.0 | 7,000.0 | 55.00 | 5.6 | 3.34 | 52.88 | 42.74 | 2.97 | 46,331.9 | 0.0882 | 11 |
| High Van Allen Gap | 12,000.0 | 12,000.0 | 55.00 | 3.5 | 3.92 | 107.90 | 84.86 | 2.11 | 65,428.7 | 0.1245 | 8 |
| Molniya | 39,850.50 | 500.00 | 63.55 | 2.0 | 130.41 | 551.70 | 479.75 | 2.01 | 351,654.4 | 0.6691 | 2 |
| GPS | 20,200.0 | 20,200.0 | 55.00 | 2.0 | 8.82 | 234.16 | 185.40 | 1.23 | 83,242.7 | 0.1584 | 6 |
| GEO | 35,786.0 | 35,786.0 | <1 | 1.0 | 0.00 | 0.00 | 0.00 | N//A | 0.00 | 0.0000 | N/A |

- Shadowing not yet considered


## Satellite Shadowing Analysis (1 of 2)

- Shadowing analysis is complicated by the fact that shadowing is often seasonally-varying
- $500 \mathrm{~km}, 28.5^{\circ}$ LEO orbit, shadowing time per orbit is roughly 28 to 36 minutes, with 35 minutes being typical; this is $37 \%$ of the 94.6-minute period
- LEO ALPHA $2158.6 \mathrm{~km}, 28.5^{\circ}$ : time in shadow typically runs from about 27 minutes through about 35 minutes. Since the satellite has a 131 minute period, the maximum shadowing time would be at most $27 \%$, often less, so a $25 \%$ estimate is reasonable
- Minimum shadowing time is zero -- that is, there are periods of several days in which the satellite is never in shadow.
- Shadowing of the satellite by the Moon occurs occasionally


## Satellite Shadowing Analysis (2 of 2)

- A previous study (Potter and Davis, 2009¹) has shown that the sun-synchronous repeating ground track orbits for the 10,11 , and 12 orbit/day cases are in sunlight continuously, and the 9 orbit/day case is in sunlight continuously, except for a few minutes/day during December
- This assumes that the ground track is over the terminator. Other orientations of the line of nodes will result in shadowing, typically 35 minutes/orbit
- A satellite in equatorial circular GEO will be in shadow for up to 72 minutes/day within a few weeks of the equinoxes, around midnight local time
- Analysis for the year under consideration also shows three incidences of a GEO SPS being in the Moon's penumbra for up to 67 minutes


## Downselection of Orbits for Constellation Analysis

- The orbits shaded in green span the trade space of reasonable solutions, and will be subjected to further analysis for constellation configuration; i.e., number of orbital planes, number of satellites per plane, and phasing of satellites between planes
- Only one plane need be considered for GEO
- Very low LEO requires too many satellites to achieve a high duty cycle early operating capability; such satellites are in shadow during a higher percentage of their orbital period than satellites in higher orbits
- Molniya orbits, while possibly desirable for high-latitude locations, are constrained by a high apogee
- System sizes will likely be similar to GEO SPS's
- CONOPS may be similar to SPS's in the CASSIOPeiA orbit
- Therefore, detailed separate consideration for Molniya may not be necessary

| Orbit Description | Apogee <br> Altitude (km) | Perigee <br> Altitude (km) | Inclination <br> (deg) | No. <br> Orbits/Day | Period <br> (min) |
| ---: | ---: | ---: | ---: | ---: | ---: |
| LEO | 500.0 | 500.0 | 28.50 | 15.2 | 94.6 |
| Sun Sync Repeat | $1,676.5$ | $1,676.5$ | 102.94 | 12.0 | 119.9 |
| LEO ALPHA | $2,158.6$ | $2,158.6$ | 28.50 | 11.0 | 130.8 |
| Sun Sync Repeat | $2,158.6$ | $2,158.6$ | 105.93 | 11.0 | 130.8 |
| Sun Sync Repeat | $2,719.9$ | $2,719.9$ | 110.06 | 10.0 | 143.9 |
| Sun Sync Repeat | $3,383.6$ | $3,383.6$ | 116.03 | 9.0 | 160.0 |
| CASSIOPeiA | 7414.00 | 963.00 | 116.60 | 8.0 | 180.16 |
| Low Van Allen Gap | $7,000.0$ | $7,000.0$ | 55.00 | 5.6 | 256.7 |
| High Van Allen Gap | $12,000.0$ | $12,000.0$ | 55.00 | 3.5 | 413.2 |
| Molniya | $39,850.50$ | 500.00 | 63.55 | 2.0 | 717.69 |
| GPS | $20,200.0$ | $20,200.0$ | 55.00 | 2.0 | 718.7 |
| GEO | $35,786.0$ | $35,786.0$ | $<1$ | 1.0 | $1,436.1$ |

## LEO ALPHA: Constellation Development

- Orbital parameters
- Altitude $=2158.6 \mathrm{~km}$
- Inclination $=28.5^{\circ}$
- Eccentricity $=0$ (circular)
- Constellation
- Type: Walker Delta with $360^{\circ}$ spread in Right Ascension of Ascending Node (RAAN)
- Number of satellites: 34
- Number of orbital planes: 17 (hence, 2 satellites per plane)
- Phase factor: 3 (thus, true anomaly difference between adjacent satellites in adjacent planes is 3 x $360^{\circ} / 34=31.76^{\circ}$
- Walker notation: $\mathrm{i}: \mathrm{t} / \mathrm{p} / \mathrm{f}=28.5^{\circ}: 34 / 17 / 3$

LEO Constellation to Ground Station Access


## LEO ALPHA: Constellation Development



## Sun-Synch 11 Orbits/Day: Constellation Development

- Orbital parameters
- Altitude $=2158.6 \mathrm{~km}$
- Inclination $=105.93^{\circ}$
- Eccentricity = 0 (circular)
- Position of initial (seed) orbit: Right Ascension of Ascending Node (RAAN) $=90^{\circ}$ at the vernal equinox; thus, initial orbit is around the day-night terminator, though the other plane in the constellation will be around the 12 midnight - 12 noon circle
- Constellation
- Type: Walker Delta, with $180^{\circ}$ RAAN spread
- Number of satellites: 18
- Number of orbital planes: 2 (hence, 9 satellites per plane)
- Phase factor: 1 (thus, true anomaly difference between adjacent satellites in adjacent planes is 1 x $360^{\circ} / 18=20^{\circ}$
- Walker notation: $\mathrm{i}: \mathrm{t} / \mathrm{p} / \mathrm{f}=105.93^{\circ}: 18 / 2 / 1$



## Sun-Synch 11 Orbits/Day: Constellation Development



## CASSIOPeiA Orbit: Constellation Development

- Orbit proposed by Ian Cash for CASSIOPeiA Solar Power Satellite
- Orbital parameters
- Apogee $=7,414 \mathrm{~km}$
- Perigee $=963 \mathrm{~km}$
- Inclination = $116.6^{\circ}$
- Argument of Perigee $=270^{\circ}$, hence, apogee is over northern hemisphere
- Eccentricity $=0.305$
- Constellation
- Type: Walker Delta, with $180^{\circ}$ RAAN spread
- Number of satellites: 8
- Number of orbital planes: 2 (hence, 4 satellites per plane)
- Phase factor: 1 (thus, true anomaly difference between adjacent satellites in adjacent planes is $1 \times 360^{\circ} / 8$ $=45^{\circ}$
- Walker notation: $\mathrm{i} \mathrm{t} / \mathrm{p} / \mathrm{f}=116.6^{\circ}: 8 / 2 / 1$
- Note: May also consider a 5-satellite, 5-plane constellation, as per lan Cash's paper


# Analysis in Progress 

## CASSIOPeiA Orbit: Constellation Development



## Conclusions

- Preliminary results have validated a methodology to span the trade space of satellite orbits and ground sites, and provide a reasonable estimate of the number of satellites required to achieve a required rectenna contact time duty cycle
- The solution space is sufficient to map on to several promising SPS concepts
- Coverage gaps may be filled by more satellites, energy storage on the ground, energy storage onboard the satellites, or some combination of these
- A comparative cost analysis can give insight into the proposed systems


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